

# A Stochastic Hole Trapping-Detrapping Framework for NBTI, TDDS and RTN

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**Abstract**—A stochastic framework is presented to model hole trapping and detrapping into and out of individual defects that are present in the gate dielectric of a p-channel MOS transistor. The model calculates thermionic reactions between uncharged and charged states of a defect that are separated by an energy barrier, by using the Gillespie Stochastic Simulation Algorithm (GSSA). The model is validated using experimental data from small area devices under Negative Bias Temperature Instability (NBTI), Random Telegraph Noise (RTN) and Time Dependent Defect Spectroscopy (TDDS) studies.

**Keywords**—GSSA, NBTI, RTN, TDDS.

## I. INTRODUCTION

NBTI is a key reliability concern in small and large area pMOSFETs [1]. The degradation and recovery of  $\Delta V_T$  during and after NBTI stress is due to the cumulative contributions from interface trap generation ( $\Delta V_{IT}$ ), hole trapping ( $\Delta V_{HT}$ ) and bulk trap generation ( $\Delta V_{OT}$ ) subcomponents. Accurate modelling of the same requires understanding the physical mechanisms that govern these processes.

Hole trapping and detrapping results in drain current and threshold voltage instabilities during NBTI, RTN and TDDS studies [2]-[4]. Historically, the Shockley-Read-Hall (SRH) mechanism is used to calculate the time kinetics [5], usually with temperature (T) activated capture cross section to account for trap relaxation and phonon coupling effects [6]. Alternatively, trap relaxation effect is handled by using thermionic [7] or non-radiative multi-phonon (NMP) [8] processes, in models that treat the uncharged and charged states of a defect as two energy levels; either separated by an energy barrier [7] or represented as intersecting parabolic potentials of a quantum harmonic oscillator [8]. Deterministic implementation of these models are used for NBTI kinetics in large area devices [9], [10], and the stochastic implementation of the multi-phonon model are used for NBTI and TDDS kinetics in small area devices [11]. Note, the original thermionic model of [7] is modified in [9] using a thermally activated barrier for explanation of NBTI stress-recovery kinetics under different T. This deterministic Activated Barrier Double Well Thermionic (ABDWT) model [9] is further validated in [12] by using NBTI stress-recovery data from diverse experimental conditions (wide stress  $V_G$  and T ranges) and different technologies. Moreover, the dependence of capture ( $\tau_c$ ) and emission ( $\tau_e$ ) times, associated with hole trapping and detrapping during TDDS and RTN on gate voltage ( $V_G$ ) is not shown in [11]. This particular aspect is addressed by the extended multi-phonon model of [4]. However large number of parameters (mean + spread = 22)

makes it hard to implement in practical situations. Moreover, explanation of NBTI kinetics (like in [12]) is not shown (yet) even using [4].

## II. SCOPE OF THIS WORK

The success of deterministic ABDWT model in explaining measured NBTI stress-recovery kinetics over wide T range ( $-40^\circ\text{C}$  to  $+150^\circ\text{C}$ ) and for multiple technologies, such as Silicon Oxynitride (SiON), Gate First (GF) High-K Metal Gate (HKMG) and Replacement Metal Gate (RMG) HKMG based planar and FinFET devices [9], [12] has motivated the stochastic version of the same in this work. The mean of multiple stress-recovery simulations matches mean NBTI kinetics measured in multiple small area devices under different stress  $V_G$  and T. The  $V_G$  and T dependence of  $\tau_c$  and  $\tau_e$  for RTN and TDDS studies can be explained. The time kinetics of individual defects during TDDS can also be explained.

## III. MODEL FRAMEWORK

The ABDWT model provides transition rates for charge (hole in p-FET) capture and emission within a trap, Fig.1. The hole capture reaction is modeled as a transition from a reference neutral state ( $E_1$ ) to the charged state ( $E_2$ ) via a barrier ( $E_B$ ). The barrier  $E_B$  and state  $E_2$  reduces when a gate bias ( $V_G$ ) is applied [12]. The barrier energy  $E_B$  is distributed in energy to model the spatial and energetic distribution of traps. For setting up the stochastic simulation, a finite number of defects are randomly distributed at the Si/oxide interface. Each defect is assigned random barrier energy  $E_B$  obtained from a normal distribution. Simulations are performed on multiple devices by invoking GSSA [13] to generate individual trapping and detrapping transients. A hole trapping (or detrapping) event manifests onto the stochastic  $\Delta V_{HT}$  transient as a positive (or negative) discrete jump. Macroscopic simulation with identical ABDWT model parameters [12] is shown to match mean of multiple stochastic simulations.

## IV. NBTI VALIDATION

Fig.2 depicts measured  $\Delta V_T$  stress kinetics from multiple small area devices of type D2 [12] at a reference stress  $V_{GSTR}$  and temperature (T) along with their mean. Mean of measured  $\Delta V_T$  kinetics is modeled by the macroscopic BAT framework [2], which isolates the subcomponents  $\Delta V_{IT}$  (generation of interface traps) and  $\Delta V_{HT}$ . It is seen that the impact of  $\Delta V_{HT}$  is relatively higher at shorter stress time and lower T whereas

$\Delta V_{IT}$  dominates at long stress time and high T. Mean of individual stochastic  $\Delta V_{HT}$  traces is shown to converge with the macroscopic model  $\Delta V_{HT}$ , Fig.3. Comparison of stochastic mean with experimental  $\Delta V_{HT}$  (mean) is performed for a range of  $V_{GSTR}$  (Fig.4) and with macroscopic  $\Delta V_{HT}$  curves for a range of T (Fig.5) to affirm the veracity of the model in a rigorous fashion. In Figs.6-9, similar treatment is accorded to the  $\Delta V_{HT}$  transients during recovery: matching of mean and macroscopic (Fig.6), isolating the mean  $\Delta V_{HT}$  from measured data (Fig.7) using BAT, and model experimental data for various  $V_G$  (Fig.8) and T (Fig.9). Fig.10 and 12 depict the measured  $\Delta V_{HT}$  time kinetics during stress and recovery respectively over an extended temperature range (-40°C to +150°C) for device type D3 [12]. The model calculated time transients are reproduced in Fig.11 and 13 and are shown to be concurrent with experimental data over the large temperature range.

## V. RTN AND TDDS VALIDATION

Fig.14 shows dependence of  $\tau_c$  and  $\tau_e$  on  $V_G$  obtained from RTN measurements at various T [3]. This is reproduced by model (Fig.15) that reveals similar T activation trends. Correlation of  $\tau_c$  and  $\tau_e$  with change in temperature [3] is depicted in Fig.16. A slope greater than 1 indicates  $\tau_e$  is more strongly coupled with T whereas a slope less than 1 suggests a stronger coupling for  $\tau_c$ . For slopes  $\sim 1$ ,  $\tau_c$  and  $\tau_e$  show equal T acceleration. These trends are modeled in Fig.17 by simulating individual traps with appropriate ABDWT model parameters to generate different T accelerations for each. Recovery step heights versus emission time plot (Fig.18) from TDDS measurement [11] for  $\Delta V_{HT}$  dominated (shorter time of stress and lower T) and  $\Delta V_{IT}$  dominated (longer time of stress and higher T) kinetics is reproduced (Fig.19).  $\Delta V_{HT}$  dominated kinetics show shorter emission times and hence recover faster. Step heights generated from the stochastic model (Fig.19) are found to be consistent with above.

Fig.20 models the  $V_G$  dependence of  $\tau_c$  and  $\tau_e$  acquired from TDDS measurements for a non-switching trap [4]. The bias dependence is reproduced across two different T using suitable model parameters for the trap. The vanilla ABDWT model is unable to reproduce the distinct tapering off of capture time constants towards saturation at higher biases, as illustrated in Fig.20. This is addressed by modifying the field activated barrier lowering by introducing a weakly quadratic dependent term in addition to the linearly dependent term which is present in the original model. The same is depicted schematically in Fig.21. The modified ABDWT model yields the correct capture time bias dependence, Fig.22. Prediction of switching trap [4] time constants is also shown using the modified ABDWT model, Fig.23. Prediction of experimental TDDS data of trap 'A1' is performed using the classical NMP transition rates in [14]. These require a correction factor to accurately model the data. In Fig.24, ABDWT is invoked to model the TDDS data of trap 'A1'.

Fig.25 enumerates the distinct types of bias couplings observed in RTN data [15]. The different  $V_G$  dependencies can be reproduced by the model upon selection of appropriate parameters.

## V. CONCLUSION

GSSA is used to implement stochastic version of the ABDWT model for hole trapping-detrapping. Experimental time kinetics for NBTI stress-recovery are accurately predicted over a range of biases, temperatures and technologies. RTN measured capture-emission time constants are reproduced and their T activation trends are captured. Switching and non-switching trap characteristics are modelled using TDDS data. Different  $V_G$  dependence of  $\tau_c$  and  $\tau_e$  of different RTN traps can be explained.

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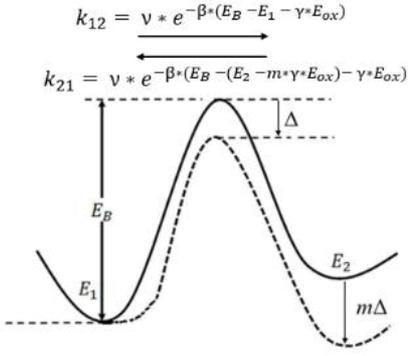


Fig.1. Schematic of ABDWT model.  $E_1$ ,  $E_2$  and  $E_b$  define the energetic configuration of the trap whereas  $m$  and  $\gamma$  control the bias coupling.

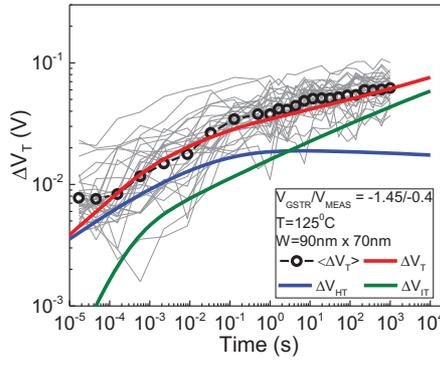


Fig.2. Individual (gray) and mean (black) measured  $\Delta V_T$  traces during stress along with model calculated mean (red) and decomposition into subcomponents

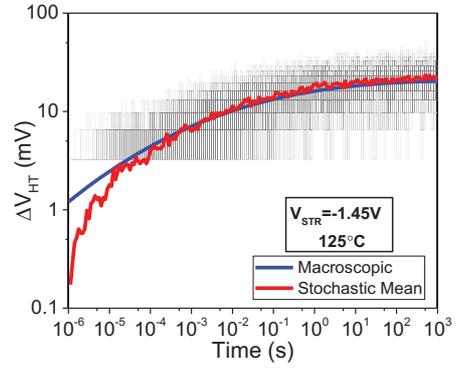


Fig.3. Individual stochastic  $\Delta V_{HT}$  stress traces (gray) and their mean alongside macroscopic  $\Delta V_{HT}$  curve.

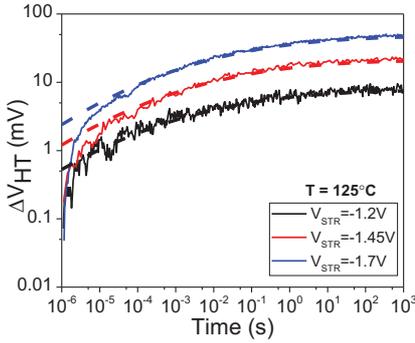


Fig.4. Matching of mean stochastic  $\Delta V_{HT}$  stress curves (solid lines) with corresponding experimental data (dashed lines) for different stress biases.

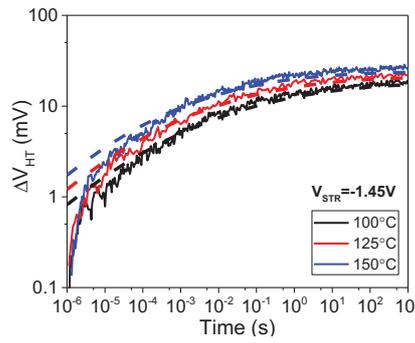


Fig.5. Matching of mean stochastic  $\Delta V_{HT}$  stress curves (solid lines) with corresponding macroscopic curves (dashed lines) at different temperatures.

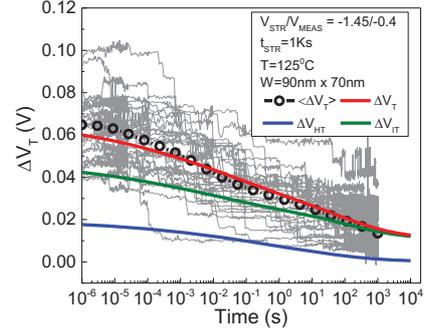


Fig.6. Individual (gray) and mean (black) measured  $\Delta V_T$  traces during recovery along with model calculated mean (red) and decomposition into subcomponents

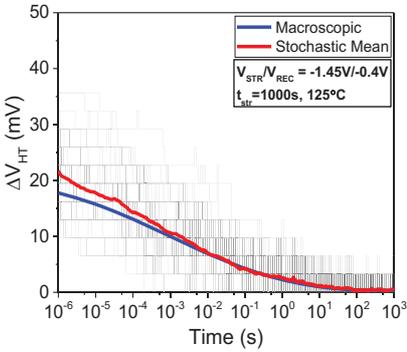


Fig.7. Individual stochastic  $\Delta V_{HT}$  recovery traces (gray) and their mean alongside macroscopic  $\Delta V_{HT}$  curve.

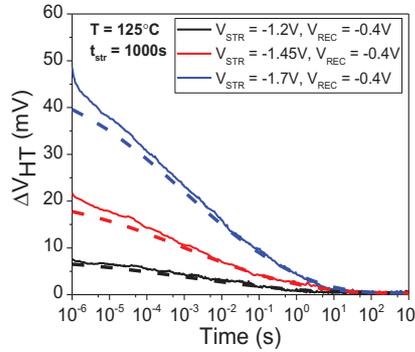


Fig.8. Matching of mean stochastic  $\Delta V_{HT}$  recovery curves (solid lines) with corresponding experimental data (dashed lines) for different stress biases.

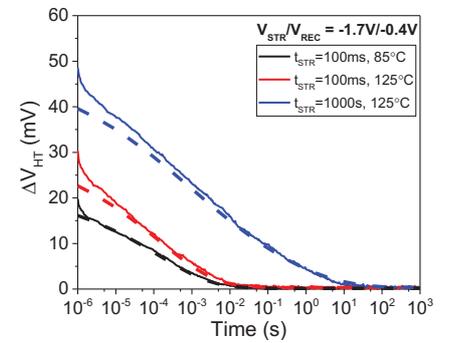
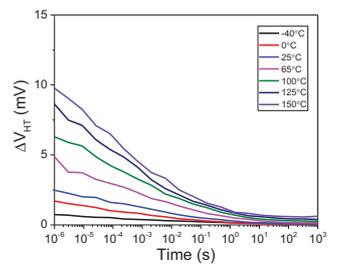
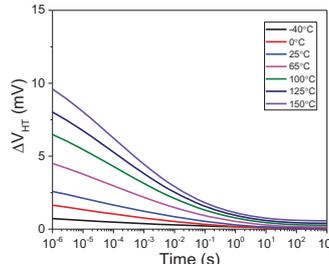
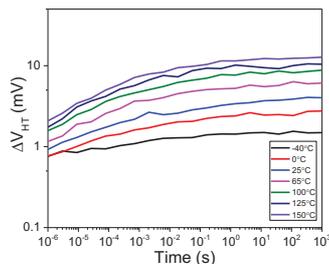
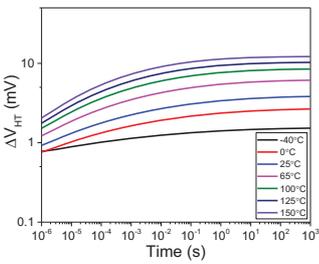


Fig.9. Matching of mean stochastic  $\Delta V_{HT}$  recovery curves (solid lines) with corresponding experimental data (dashed lines) for different stress time and temperature.



Figs.10-13. Comparison of mean stochastic  $\Delta V_{HT}$  degradation with experimental data over extended temperature range. Stress and recovery curves are generated and shown to be consistent with measured data. Device is type D3 (RMG HKMG SOI FinFET).

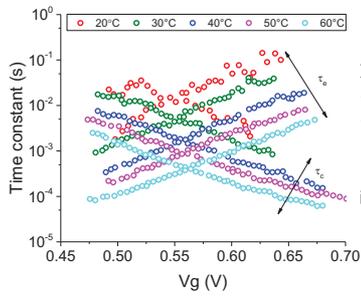


Fig. 14. Time constants as a function of  $V_G$  at various temperatures from RTN experiments [3].

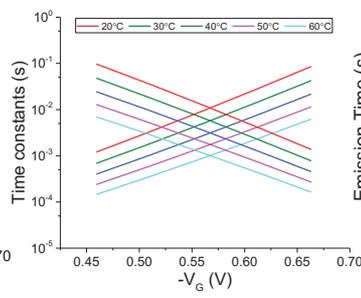


Fig. 15. Simulated time constants as a function of  $V_G$  at various temperatures.

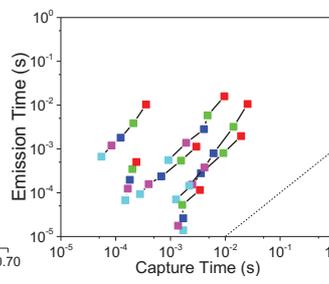


Fig. 16. Time constant traces with change in temperature from RTN experiments [3].

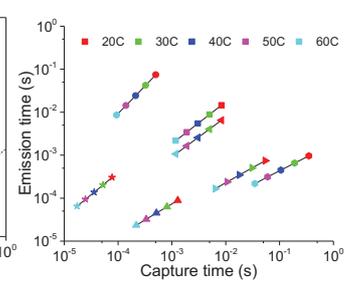


Fig. 17. Simulated time constant traces with change in temperature. By suitably choosing model parameters, a wide range of slopes may be obtained.

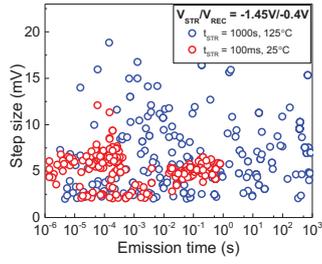


Fig. 18. Measured  $\Delta V_T$  step height versus emission time from TDDS recovery traces.

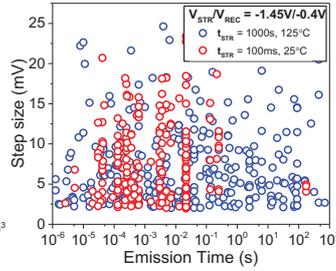


Fig. 19. Simulated step height versus emission time generated from stochastic  $\Delta V_{HT}$  recovery traces.

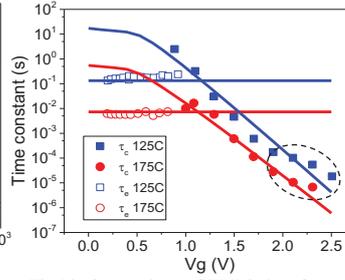


Fig. 20. Comparison of TDDS data for non-switching trap [4] (symbols) with model calculated time constants (lines). Model calculation predicts linearly decreasing capture time constant whereas experimental results show tapering off towards saturation at higher biases.

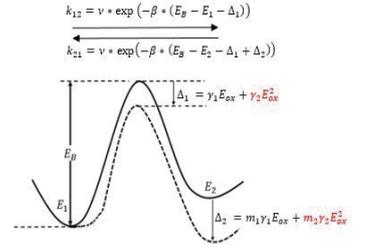


Fig. 21. Modified ABDWT schematic diagram. At low biases barrier lowering is linear in Eox while at higher biases it becomes quadratic.

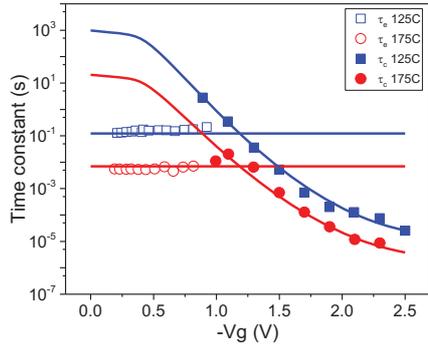


Fig. 22. Simulated capture times using the modified ABDWT correctly predicts the tapering off of time constants at higher biases.

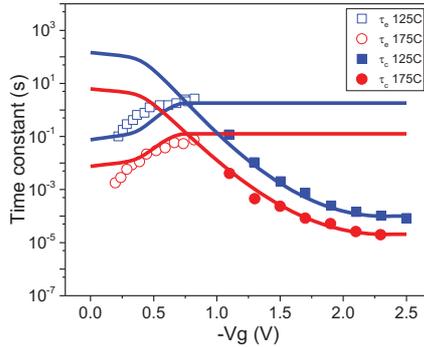


Fig. 23. Prediction of TDDS capture and emission time constants (symbols) for switching trap [4] using modified ABDWT (lines).

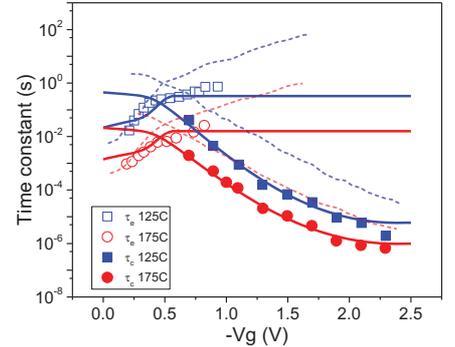


Fig. 24. Comparison of TDDS data for trap 'A1' [14] (symbols) with ABDWT model calculated time constants (solid lines) as well as NMP calculated time constants (dashed lines).

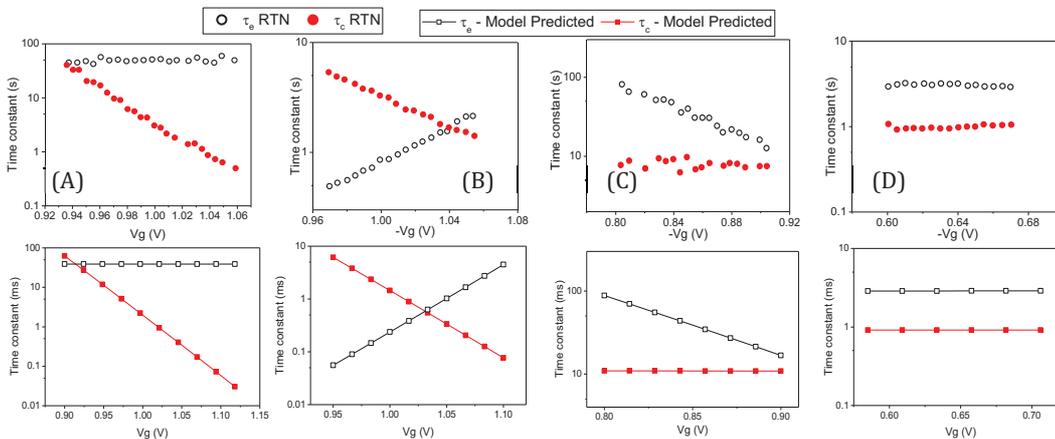


Fig. 25. Upper panel depicts various couplings of time constants to  $V_G$  extracted from RTN data [15]. (A)  $\tau_c < 0$ ,  $\tau_e \sim 0$ , (B)  $\tau_c < 0$ ,  $\tau_e > 0$ , (C)  $\tau_c \sim 0$ ,  $\tau_e < 0$ , (D)  $\tau_c \sim 0$ ,  $\tau_e \sim 0$ . Lower panel shows time constants extracted from ABDWT model simulation. Suitable selection of ABDWT model parameters  $m$  and  $\gamma$  yields the corresponding bias couplings: (A)  $m \sim 1$ , (B)  $m > 1$ , (C)  $m < 0$  with small  $\gamma$ , (D)  $m \sim 1$  with small  $\gamma$ .