

Application of an Algebraic Multigrid Solver to Process Simulation Problems

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Abstract - In this paper, the performance of a special algebraic multigrid (AMG) solver for the solution of stress analysis problems in process simulation has been investigated. The discrete stress analysis equations are generated directly by the process simulator. The practical simulation examples include stress analysis during natively growing and deposited material films. It is shown that approaches using the AMG solver as a preconditioner are better than standard iterative solvers, regarding computing times and convergence behavior. A further comparison demonstrates that these AMG approaches are faster than the direct solver SuperLU.

I. INTRODUCTION

The semiconductor process simulation involves generally two principal classes of PDE problems. The first one is related to the redistribution of dopants and point defects in thermal processes and requires the solution of multi-particle drift-diffusion-reaction equations. The second class of problems is related to the mechanical deformation of fabricated multi-layer material structures. The corresponding governing equations account for the distribution of the stresses and strains that develops in different material regions during fabrication. However, the second class of problems is due to the elliptic nature of the governing equations, more critical for the application of classical iterative solvers facing the problems of bad conditioning. On the other side, with the growing complexity of industrial applications, direct solvers are approaching the problem of an unacceptable number of floating point operations.

It is well known that multigrid methods offer the prospect of optimal scaling the problem size. Standard multigrid methods have been already recognized as an efficient solving technique for process simulation problems if the underlying

grid structures possess a natural hierarchy resulting from a local grid refinement [1]. However, the evolving geometry of the deformed multi-layer material regions in semiconductor fabrication is generally quite irregular. The unstructured grids describing such a geometry are typically not coarse enough to serve as the coarsest grid level in multigrid algorithms. This fact has significantly limited the applicability of multigrid methods in the process simulation. A promising approach to eliminate this deficiency is the usage of algebraic multigrid methods [2,3].

The main objective of this paper is to investigate the capability of an AMG solver to cope with discretized systems of the stress governing equations occurring in the semiconductor process simulation where standard iterative solvers (preconditioned BiCG and GMRes) have non-optimal convergence behavior.

II. PROBLEM FORMULATION

Test problems for the numerical experiments are generated by the process simulator FLOOPS [5]. The stress analysis in FLOOPS, and generally in process simulation, is essentially based on the momentum equation

$$-\nabla \cdot \sigma_d + \nabla p = \mathbf{f} \quad \text{in } \Omega \quad (1)$$

where Ω is a bounded domain with boundary Γ , σ_d is the symmetric deviatoric stress tensor, p is the mean pressure and \mathbf{f} is the body force. The boundary conditions are given by

$$(-p\mathbf{I} + \sigma_d) \cdot \mathbf{n} = \mathbf{g} \quad \text{on } \Gamma_g \quad (2)$$

$$\mathbf{u} = \mathbf{h} \quad \text{on } \Gamma_u, \quad (3)$$

where \mathbf{g} is the surface traction of the boundary segment $\Gamma_g \subset \Gamma$, \mathbf{h} is the displacement of the boundary segment $\Gamma_u \subset \Gamma$ ($\Gamma_u \cap \Gamma_g = \emptyset$), and \mathbf{n} is the outward unit normal vector on the boundary. Mechanical properties of the materials involved in the semiconductor fabrication are varying from purely elastic solids to viscous fluids and therefore quite accurately modelled with the constitutive relationship of the Maxwell viscoelasticity. The Maxwell viscoelasticity is commonly implemented in process simulation in its incremental form based on the constitutive relationships of linear elasticity

$$\boldsymbol{\sigma}_d = 2G_{\text{eff}} \left[\frac{1}{2} (\nabla \mathbf{u} + \nabla \mathbf{u}^T) - \frac{1}{3} (\nabla \cdot \mathbf{u}) \mathbf{I} \right] \quad \text{in } \bar{\Omega} \quad (4)$$

$$p = -K \nabla \cdot \mathbf{u} \quad \text{in } \bar{\Omega} \quad (5)$$

where the viscoelastic material properties are introduced by an effective shear modulus G_{eff} given by

$$G_{\text{eff}} = G \frac{\tau}{\Delta t} \left(1 - \exp \left(-\frac{\Delta t}{\tau} \right) \right). \quad (6)$$

Here \mathbf{u} is the incremental displacement vector, $G > 0$ and $K > 0$ are the shear and bulk moduli, \mathbf{I} is the identity tensor, Δt is the time step size, and τ is Maxwellian relaxation time defined as $\tau = \mu/G$, where μ is the material viscosity. Notice that G_{eff} provides a continuous modelling of the material mechanical behavior from the purely elastic deformation to the viscous flow. Namely, for $G \ll \mu$ it reduces to the Hooke's law for the elasticity while for $\mu \ll G$, we obtain the Newton law for the viscous fluids.

The stress governing equations are discretized using standard piecewise linear Galerkin finite elements.

III. ALGEBRAIC MULTIGRID

Today a lot of different algebraic multigrid approaches exist. We here refer to a very flexible, robust and efficient approach in practice. It has been implemented in the code SAMG16 (called AMG below), a further development of RAMG05 [3] for PDE systems, which incorporates more efficient and more flexible interpolation and coarsening strategies than its predecessor AMG1R5. But because the research version we have used is under permanent development it is not optimized especially in terms of computing times, and substantial improvements can be expected for a "final version".

Belonging to the group of multi-level methods, AMG is designed to solve certain types of sparse-matrix equations such as those typically arising from the discretization of elliptic partial differential equations (PDEs) or structurally similar problems. Although it employs the ideas of smoothing and coarse grid correction it works different than geometric multigrid and uses only information contained in the given matrix, and additionally in the case of a discretized system of PDEs simple informations about unknown-point-variable relations. Therefore it is especially suited for problems based on unstructured grids.

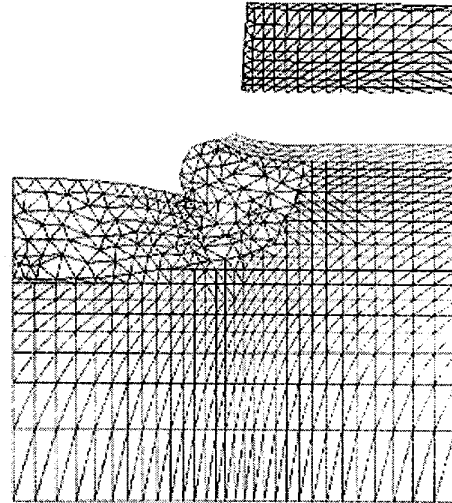


Figure 1: The grid structure for the SILO isolation problem.

For the same reason there is no need to completely restructure existing software packages: AMG can be seen as a kind of "plug-in" or "black box" solver.

For large classes of problems AMG is an efficient alternative to standard numerical iterative methods such as conjugate gradient (CG) or BiCGstab accelerated by typical (one-level) preconditioners. AMG can handle millions of unknowns and shows better convergence rates, to a large extent independent of the size of the given problem. Often the efficiency can be increased further by using (cheaper, low-memory) AMG variants as a preconditioner for GMRes or BiCGstab. There is also the possibility to parallelize AMG which has been shown by recently developed versions [4].

The classes of problems, AMG has successfully been applied to, include for example problems on very complex, unstructured grids (e.g. industrial CFD applications) and problems with strongly anisotropic and discontinuous coefficients (e.g. oil reservoir simulation). But most of these cases require after all the solution of a single partial differential equation. Although the AMG approach has already successfully been used for solving various types of PDE systems, the development has not yet reached a state where a particular approach is well-settled.

IV. NUMERICAL RESULTS

A. Comparison of different iterative approaches

The basic iterative approaches and their preconditioners, which are used for solving the created problems, are listed in Table I.

We have considered three practical text examples in our numerical experiments. The first one corresponds to the "sin-

gle full integration stress solving step” in the simulation of the “Sealed Interface Local Oxidation” (SILO) process. The underlying grid structure is shown in Fig. 1. The next two simulation examples, (DEPO1) and (DEPO2) are related to the stress distributions in multilayer material regions after thin film deposition processes. The origin of the stress are intrinsic stress distributions in the deposited material films.

Results of numerical tests with the SILO and the DEPO examples are given in Tables II to IV. AMG-GM20 and AMG-GM4 are the fastest approaches (for an residual reduction of 10 orders of magnitude). Especially for the DEPO examples AMG-BiCG reduces the residuals exceptionally well, and although two AMG steps are used for preconditioning, for a residual reduction by more than 10^{10} it is faster than AMG-GM.

The approaches with AMG as preconditioner show much better ARFs than the other approaches tested. AMG as a stand-alone solver is much better than GM4 and has a better ARF than GM20, but it is slower than BiCG and GM20 (exception: DEPO2). For the SILO example AMG has a worse ARF than BiCG, for the DEPO examples it is vice versa.

As last example (NMEx), we have considered the stress distribution in a material consisting of four blocks, whose structure can be seen in Fig. 2. We have used three triangulations with different numbers of elements.

Tables V to VII show similar results than the first three examples. AMG-GM20 and AMG-BiCG give the fastest total run times and best ARFs (but worse than those in the SILO example). AMG as a stand-alone solver reduces the residuals only a little bit better than GMRes but worse than BiCG, and for a residual reduction of 10 orders of magnitude it is slower than BiCG and GM20 (for larger numbers of variables).

By looking at the residual development one can see that both BiCG and GMRes show residual reduction rates close to or even larger than 1 in some steps and a partially oscillating behavior, but the residual reduction factors for AMG (as a stand-alone solver) increase monotonously, at first in quick steps, then slowly, and converge against a final value smaller than, but close to 1. For both cases the conclusion can be drawn that the iteration matrices have some eigenvalues close to 1, and therefore the approaches are not able to reduce the parts of the error that belong to the corresponding eigenvectors.

AMG as a preconditioner for BiCGstab or GMRes improves the spectral radius of the corresponding iteration matrix somewhat. The residual reduction rates are bounded away from 1 but are varying.

Although AMG-BiCG or AMG-GM (example dependent) are the best approaches for the problems tested, it is obviously necessary to improve the capability of the AMG solver to cope with discretized systems of PDEs or structurally similar problems, e.g. by preconditioning the matrices to be solved in consideration of the special system structure.

B. Comparison with SuperLU

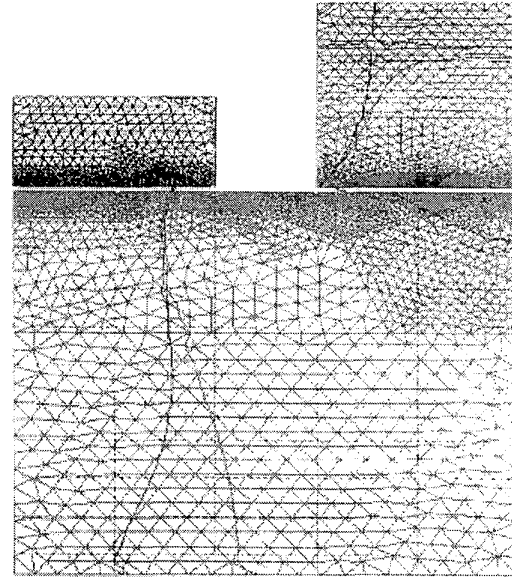


Figure 2: The grid structure (and some of the solution contour lines) for the NMEx problem with 8954 variables (blue=nitride, green=oxide, yellow=polysilicon, cyan=silicon).

To get a first impression how fast the AMG approaches are, we have compared AMG-BiCG to the direct solver SuperLU (a fast incomplete LU factorization built into FLOOPS) by measuring total wall-clock times for computing the solution (including grid generation). The results, which are shown in Table VIII, are of great promise, particularly because SAMG16 can be optimized further.

V. CONCLUSION

In summary the numerical experiments have demonstrated the following: The usage of the AMG solver SAMG16 as a preconditioner for BiCGstab or GMRes (with a large dimensional Krylov space) results in approaches which are better than the standard iterative solvers BiCGstab and GMRes which are currently used in process simulation tools. The AMG approaches are faster and their convergence rates are smaller and more stable. Since the benefits of AMG solvers increase with the problem size and since SAMG16 can be optimized and developed further, it can be expected that AMG could play an essential role in the next generation of process simulation tools.

REFERENCES

- [1] W. Joppich and S. Mijalković, *Multigrid Methods for Process Simulation*, Springer-Verlag, Wien New York, 1993.

TABLE I
DESCRIPTION OF THE DIFFERENT APPROACHES

Name	Basic approach ^a	Preconditioner ^b
AMG	standard AMG	none
AMG-BiCG	BiCGstab	2 AMG it
BiCG	BiCGstab	ILUT(9)
AMG-GM20	GMRes(20)	1 AMG it
GM20	GMRes(20)	ILUT(9)
AMG-GM4	GMRes(4)	1 AMG it
GM4	GMRes(4)	ILUT(3)

^aGMRes(x): x=dimension of the Krylov space

^bit=iteration(s)

TABLE II
RESULTS FOR THE SILO EXAMPLE WITH 1810 VARIABLES AND 23079 NON-ZERO MATRIX ENTRIES: AVERAGE RESIDUAL REDUCTION FACTORS (ARF), NUMBER OF CYCLES NEEDED TO REDUCE STARTING RESIDUAL BY 10^{10} AND RUN TIME (IN SECONDS).

Approach	ARF	cycles	time
AMG-GM4	0.265	18	0.36
AMG-GM20	0.250	17	0.37
BiCG	0.519	36	0.39
GM20	0.744	78	0.52
AMG-BiCG	0.199	15	0.54
AMG	0.537	38	0.63
GM4	0.846	138	0.82

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- [4] A. Krechel and K. Stüben, *Parallel Algebraic Multigrid Based on Subdomain Blocking*, GMD Report 71, December 1999.
- [5] M. E. Law, *Florida Object-Oriented Process Simulator, FLOOPS/FLOODS Manual*, University of Florida, Gainesville, 1993.

TABLE III
RESULTS FOR THE DEPO1 EXAMPLE WITH 1432 VARIABLES AND 15912 NON-ZERO MATRIX ENTRIES

Approach	ARF	cycles	time
AMG-GM20	0.117	11	0.22
AMG-GM4	0.123	12	0.23
AMG-BiCG	0.016	7	0.26
BiCG	0.340	25	0.27
GM20	0.634	51	0.28
AMG	0.267	18	0.42
GM4	0.955	505	1.65

TABLE IV
RESULTS FOR THE DEPO2 EXAMPLE WITH 3224 VARIABLES AND 38425 NON-ZERO MATRIX ENTRIES

Approach	ARF	cycles	time
AMG-GM20	0.211	15	1.86
AMG-GM4	0.239	17	1.90
AMG-BiCG	0.052	9	2.04
BiCG	0.553	39	2.13
AMG	0.475	31	2.95
GM20	0.824	119	4.15
GM4	0.985	1526	29.96

TABLE V
RESULTS FOR THE NME1 EXAMPLE WITH 8954 VARIABLES AND 121868 NON-ZERO MATRIX ENTRIES

Approach	ARF	cycles	time
AMG-GM20	0.344	22	8.0
AMG-BiCG	0.174	14	9.3
AMG-GM4	0.528	37	12.0
BiCG	0.749	82	13.5
AMG	0.854	146	38.6
GM20	0.949	437	44.6
GM4	0.990	(1000) ^a	(64.7) ^a

^aResidual reduction by a factor of 10^4 only.

TABLE VI
RESULTS FOR THE NME2 EXAMPLE WITH 16836 VARIABLES AND 230896 NON-ZERO MATRIX ENTRIES

Approach	ARF	cycles	time
AMG-GM20	0.498	34	23.6
AMG-BiCG	0.273	18	24.2
BiCG	0.812	118	37.3
AMG-GM4	0.742	78	48.3
GM20	0.953	483	99.9
AMG	0.947	422	210.9
GM4	0.996	(2000) ^a	(288.9) ^a

^aResidual reduction by a factor of 10^5 only.

TABLE VII
RESULTS FOR THE NME3 EXAMPLE WITH 21794 VARIABLES AND 299593 NON-ZERO MATRIX ENTRIES

Approach	ARF	cycles	time
AMG-BiCG	0.251	19	34.3
AMG-GM20	0.523	36	36.3
BiCG	0.837	130	55.5
AMG-GM4	0.749	80	66.0
GM20	0.962	597	158.2
AMG	0.950	449	297.8
GM4	0.996	(2000) ^a	(380.8) ^a

^aResidual reduction by a factor of 10^5 only.

TABLE VIII
WALL-CLOCK TIMES FOR COMPUTING THE SOLUTION WITH SuperLU AND AMG-BiCG (IN MINUTES)

Example	NME2	NME3
AMG-BiCG	1:37	2:26
SuperLU	2:26	3:13