Electric Response of Ovonic Materials to Oscillating Potentials

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Abstract—This paper presents a computational analysis, by means of a compact model, of the electric response of an Ovonic Threshold-Switch device embedded in a circuit subjected to an oscillatory bias.

I. INTRODUCTION

Ovonic threshold switch (OTS) and phase-change materials have been selected by some leading electronic industries as semiconductors for innovative devices in the field of data storage, and proposed for beyond-von Neumann calculators and bio-inspired neuromorphic computing. Recently, planar arrays of chalcogenide-based devices have been realized, and commercial mass production has been announced. This paper addresses the issue of the single OTS-device response to oscillating potentials.

The $I(V)$ curve of an Ovonic device exhibits two stable states featuring different resistivities, with a typical S-shaped current-voltage characteristic [1], [2], [3], [4], [5]. Most investigators agree in ascribing the above behavior to hot-carrier phenomena [6], [7]; according to this interpretation, different carrier temperatures are at the origin of the two resistivity states. It must be remarked that most of the electrical analyses published in the literature refer to steady-state conditions; only recently, experimental evidence pointed out that the transient features related, e.g., to how the bias is applied [8] or to the recovery time after the bias is changed [9], introduce new issues about the switching process. The new physical phenomena that appear in dynamic conditions are relevant for the design of high-speed devices when the switching dynamics becomes fast enough to couple significantly with the microscopic times intrinsic to the semiconductor, and/or with the characteristic times of the external circuitry.

II. MODEL

The analysis is based on the model of [10], [11], which assumes a trap-limited transport scheme. Two energy levels are available for the carriers, separated by an energy gap $\Delta E_0 = E_B - E_T > 0$. Electrons in the deep trap states $E_T$ do not contribute to the electric current; those in the upper level $E_B$, which mimicks shallow trap states and band states, are mobile. The device is one dimensional and spatially uniform, and the total carrier concentration $n = n_B + n_T$ is fixed. The transport equations (1–3), whose unknowns are the concentration $n_B$ and temperature $T_e$ of the band electrons, are coupled to the circuit equation (4); they describe time-dependent situations with a limited computational load. The microscopic parameters appearing in the constitutive equations of the model are fixed through comparisons with existing steady-state and transient experimental data [11]. The model equations read

$$\tilde{n}_B = \frac{n}{1 + \Gamma \exp\left(\frac{\Delta E_0 - \gamma |F|}{k T_e}\right)}, \quad (1)$$

$$\frac{dn_B}{dt} = \frac{n_B - \tilde{n}_B}{\tau_N}, \quad \frac{d\epsilon}{dt} = J = q \mu e n_B F, \quad (2)$$

$$\frac{dI}{dt} = \frac{V - F L + C R_S dV/dt - I (R_S + R_L)}{C R_S R_L}, \quad (3)$$

Equ. (1) provides the steady-state, non-equilibrium concentration of the band electrons; the term $\gamma |F|$ accounts for the traps’ edge lowering due to Poole’s effect [6], [7]. The first and second equations in (2) are the continuity and transport equation for the band electrons, respectively, while equation (3) is the continuity equation for the band-electron energy $\epsilon$. Finally, (4) is the circuit’s equation. The meaning of the other symbols in (1–4) is given in Tab. I and Fig. 1.

In the steady-state condition it is $n_B = \tilde{n}_B$. Also, using in the steady-state form of (3) the expression of $J$ obtained from the
second equation in (2), and defining the constant electric field \( F_0 = \sqrt{\frac{kT_0}{q\mu T\tau}} \), one finds
\[
\frac{T_e}{T_0} = 1 + \frac{n_B}{n} \frac{F^2}{F_0^2}.
\]
(5)

It follows that in steady state it is \( T_e \geq T_0 \). By the same token, one recasts (1) as \( n/n_B = 1 + \Gamma \exp\left(\frac{\Delta E_0 - \gamma |F|}{(kT_e)}\right) \), to find that the steady-state limits of \( n_B \) are given by
\[
1 < \frac{n}{n_B} \leq 1 + \Gamma \exp\left(\frac{\Delta E_0}{kT_e}\right).
\]
(6)

In a one-dimensional, uniform material, the device voltage and current are given by \( LF, AJ \), with \( A \) the device’s cross-sectional area. Thus, to find the steady-state characteristic of the Ovonic device it suffices to determine the relation between \( F \) and \( J \). This is accomplished in parametric form, after inverting (1) and taking \( kT_e \) from (5):
\[
\frac{\Delta E_0 - \gamma |F|}{kT_0 \log((n/n_B) - 1/\Gamma)} = 1 + \frac{n_B}{n} \frac{F^2}{F_0^2}.
\]
(7)

Solving (7) as a second-degree equation in \( |F| \), one determines the \( F(n_B) \) relation (being \( F \) spatially uniform, its sign is always determined). Then, by successively giving \( n_B \) all values fulfilling (6), one uses the relation just found to calculate \( F \), while the value of \( J \) corresponding to it is given by \( J = q\mu n_B F \). The steady-state \( I(V) \) curve of Fig. 2 has been determined in this way.

III. RESPONSE TO A PERIODIC VOLTAGE

The low- and high-resistance states of an Ovonic device are important for controlling the access features to a phase-change memory bit in cross-point array architectures [12]. Thus, in view of the technological application it is necessary to assess the conductive state of the device. In this section we test the response of the Ovonic device in a circuit subjected to a periodic voltage. As expected, the device response depends on how the material’s and circuit’s characteristic times compare;

| \( n \) | Total electron concentration (band+traps) |
| \( \Gamma \) | Normalized density of states of the band |
| \( \Delta E_0 \) | Band-trap energy difference |
| \( F \) | Electric field |
| \( q \) | Absolute value of the electron charge |
| \( k \) | Boltzmann constant |
| \( T_e \) | Electron temperature |
| \( T_0 \) | Equilibrium temperature |
| \( \tau_{\eta} \) | Relaxation time of the band electrons |
| \( \tau_{\nu} \) | Relaxation time of the band electrons’ energy |
| \( \mu \) | Mobility of the band electrons |
| \( J \) | Current density across the Ovonic device |
| \( \gamma \) | Poole’s effect parameter |
| \( L \) | Length of the Ovonic device |

also, depending on the frequency and amplitude of the applied voltage, different electric regimes may set in.

The curves in Fig. 2 show the current response of the Ovonic device to an applied voltage of the form \( V(t) = (V_0/2) [1 - \cos(2\pi t/T)] \), with \( V_0 = 1.2 \) V, for different values of the period \( T \). The latter ranges from 10 ps to 10 ns. The device parameters are taken from experiments [8]: \( R_L = 50 \) \( \Omega \), \( C = 150 \) fF (hence \( \tau_C = 7.5 \) ps); moreover, we assumed
\( \tau_T = 0.15 \) ps, \( \tau_n = 0.1 \) ps. Under these bias conditions (note that the limits of \( V \) are 0 and \( V_0 \)) the Ovonic device is voltage driven, and the working point oscillates between the lower and upper branches of the static \( I(V) \) curve; no internal oscillations set in. Furthermore, for the case in hand, the characteristic time associated to the parasitic elements of the circuit, \( \tau_{C} = R_L C \), turns out to be much larger than the relaxation times controlling the internal dynamics of the device; due to this, the time needed to charge/discharge the parasitic capacitance prevails over the internal dynamics.

Fig. 3 shows the voltage and current across the device, and the corresponding band-electron temperature, as functions of time for two periods among those used in Fig. 2. As apparent in the latter figure, the switching event sets in for \( T = 100 \) ps; in the \( T = 60 \) ps case, in contrast, no switching event occurs. Also, the \( I(V) \) curve corresponding to \( T = 60 \) ps barely reaches the threshold voltage, then reverts onto itself. This outcome may qualitatively be ascribed to the shunting effect of capacitor \( C \): such an effect increases with frequency and, as a consequence, the voltage drop across \( R_L \) is larger at \( T = 60 \) ps than in the \( T = 100 \) ps case. The different response is due to the interplay between the charging/discharging time of the parasitic capacitor and the characteristic times of the internal dynamics: when \( T = 60 \) ps, the field exceeds the threshold values for a relatively short time, and the corresponding temperature (lowest box of Fig. 3) is insufficient to trigger a switching event. The opposite happens when \( T = 100 \) ps.

When the period \( T \) of the applied bias is large, i.e., the device voltage changes little during a time of the order of \( \tau_{C} \), the current through the Ovonic device follows the static \( I(V) \) curve and the voltages corresponding to the switching events coincide with the threshold and holding voltages of the latter (see, e.g., the \( T = 10 \) ns curve in Fig. 2). Switching events may also occur at shorter periods, provided the applied voltage is such that the capacitor is charged to a voltage larger than the static threshold voltage for a time long enough to produce carrier heating. In this situation, the delay due to the internal dynamics of the material shifts the switching voltage to higher values and the holding voltage to lower values (\( T = 100 \) ps curve in Fig. 2).

As noted above, no switching events occur when the period of the applied voltage becomes shorter (\( T = 60 \) ps and \( T = 10 \) ps curves in Fig. 2 for the case considered here). The qualitative analysis given earlier would be exact if the circuit were linear; in the present case, as the non-linearity of the Ovonic device introduces harmonics in addition to the fundamental frequency of the applied bias, the qualitative analysis must be corroborated by numerical results. The non-linear behavior of the device is evident in the current’s waveform (center graphs of Fig. 3); besides that, the amplitude of the device voltage and, on a much larger scale, of the device current, decreases when the applied voltage’s period decreases. This confirms the qualitative analysis carried out earlier, and reflects into the behavior of the band-electron temperature \( T_e \) shown in the lower graphs of the figure. In the \( T = 60 \) ps case the Ovonic material, still oscillating, remains in the lower branch of the \( I(V) \) curve, and \( T_e \) keeps close to its equilibrium values.

At even higher frequencies of the applied voltage, the capacitance damps the response of the Ovonic material, progressively reducing the amplitude of its voltage oscillations around the bias average value, as shown in Figs. 4 and 5.

IV. CURRENT-DRIVEN OPERATION

In this section we consider the case where the bias voltage is applied through a very large series resistance, in such a way that the Ovonic device is essentially current driven. Besides using the same relaxation times as those reported in Sect. III, here we assume \( R_L = 100 \) k\( \Omega \), \( R_S = 1 \) k\( \Omega \), and different values for the capacitance \( C \). The applied voltage has the
same form as in Sect. III, with $V_0 = 10 \text{ V}$ and $T = 1 \text{ ns}$. Of particular interest are the cases where the upper working point of the device, during its oscillations, reaches the region of the static $I(V)$ curve where the differential resistance is negative (Fig. 6). The frequency of the applied voltage is small enough to allow for the setting up of the Ovonic oscillations, evidenced also in static conditions [11]. A stability analysis in the neighborhood of the working point, i.e., after linearizing the equations, was presented in [13]; here, a full large-signal analysis is tackled.

Fig. 7 shows the time variation of the Ovonic potential and current at different values of the capacitance, ranging from 150 to 0.15 fF. As expected, the frequency of the intrinsic oscillations increases as the capacitance decreases; when the capacitance decreases even further, the working point becomes stable and the oscillations extinguish (dashed curves in the upper and lower graphs of Figs. 7, corresponding to $C = 0.15 \text{ fF}$).

V. CONCLUSIONS

In this paper, the model of [10], [11] has been used to identify different oscillating features of Ovonic Threshold-Switch devices by varying the details of the external bias and circuit elements, with the purpose of specifying about their influence on the performance of chalcogenide-based electronic products embedded into new-generation memory architectures. With respect to previous approaches, here the analysis has been extended to the case of an oscillating applied bias and to the large-signal case.

The outcome of the simulations shows how the features of the characteristic curves depend, besides the external bias, on the interplay between the material’s intrinsic times and the unavoidable parasitic elements of the circuit. In the current-driven operation, either stable or oscillating solutions are found according to the load-line dynamics and the value of the parasitic capacitance. The results reveal the high-frequency oscillation potency of Ovonic materials, which can be exploited in the design of selector devices for two-terminal Non-Volatile Memories.

REFERENCES